



Flight Test Society of South Africa

Flight Test Report Focke Wulf Piaggio P149D-TP



IASSA 2015

Des Barker



Scope



- Executive Summary of Flight Test Programme:
 - Background
 - Objectives of Test Programme
 - Scope of Modifications
 - Flight Test Team
 - Conditions Relevant
 - Results and Discussion
 - Conclusions
 - Recommendations
 - Lessons learned and observations





Background



- Designed, developed by Piaggio & Co, Italy, 1953.
- Licence built Focke Wulf: Basic trainer + light utility.
- Retired 1970 from Service.
- Acquired and imported into RSA Werner Heiml.
- Flight test NTCA 2013.





From This!



Piaggio P149D

To This!!



Focke Wulf Piaggio P149D - TP



Objectives

To demonstrate the modified *Piaggio P149D TP* aircraft's compliance with the requirements of Part 24 of the CAR's and certain applicable requirements of *FAR-23 Subpart B: Flight*.

The aircraft is a Non-Type Certificated Aircraft (NTCA) Ex-Military in terms of Part 24 of the SA Civil Aviation Regulations (CAR's).

Proving Authority. The P149D aircraft with registration ZU-SFP (S/N 0060) was operated with a Proving Flight Authority issued by the SA Civil Aviation Authority. ZU-SFP was assigned as the prototype test aircraft.

Aircraft Modifications



Basic Autopilot

O₂ System

• Dorsal Fin

• Canopy

- Lowered 125mm
- Streamlined

– ‘Swooplets’

Fuel System

- Outboard
- Mid span
- Ferry Tank

Nose U/C

720 shp Walter 601D Turboprop vs
275 hp Lycoming GO-480

- New engine mounting 600 mm/CG
- Brackets & skin doublers
- FAR23.631 structural compliance = 3.8g



Cockpit Modifications





Walter 601D TurboProp



Walter M601D Engine

- designed for remote/rugged operations.
- minimal field maintenance requirements
- Maintenance between overhauls:
 - primarily filter and screen cleaning,
 - compressor wash,
 - oil change,
 - borescope inspection,
 - igniter replacement.
- "hot section inspections" between overhauls not required.
- Recommended (TBO) defined by "cycles"
 - engine starts,
 - flight time, and
 - calendar time.
- TBO interval 2,250 to 20,000 cycles (depending service type/engine series),
- 1,500 to 3,000 hours flight time,
- 5 to 8 years calendar time between overhauls.

Cost Comparison
Walter RM1.2 vs PT-6 RM 3.5



Max. Continuous Rating	657 eshp
N₁ (Gas generator) RPM (100%)	36,293 rpm
Max. Propeller RPM	2080 rpm
Max. Inter-Turbine Temperature (ITT)	690°C
Equivalent Specific Fuel Consumption (ESFC)	0.648
Max. Fuel Consumption @ 657 eshp	65 gph
Cruise " " @ 350 to 400 eshp	35-37gph
Idle " "	25 gph
Weight (dry)	425 lb
Height/width/length (inches)	26"-23"-66"



Aeromechanical Implications



- Mass Re-distribution. Static margin maintained for standard Piaggio P149D = propeller mounting face forward by 305mm (12 inches).
- Static Margin. Net effect = mass redistribution with static margin theoretically unchanged; pitch/yaw inertial moments impacted on the static and dynamic stability characteristics of the aircraft.
- Inertial Effects. Increased propeller mass increased rotational inertia by 26% - although rotational speed essentially same as Lycoming, propeller gyroscopic loads changed.
- Power Effects. Walter 601D maximum power 2.5x greater than Lycoming GO-480
 - double propeller/engine torque
 - increased helical airflow around fuselage
 - static and dynamic stability characteristics of the aircraft changed.
- Aircraft Performance. 32% increase in shaft horse power significantly increased aircraft performance, viz SEP ie takeoff, climb, acceleration, sustained turn pfx.
- Stability and Control. Increased shaft horse power significantly increased slipstream, downwash, and mass flow – determine in flight test.





Test Programme Management Team

Test Pilot Class I. Des Barker, military (SAAF) experimental test pilot - 56 types: Piaggio P149 D, total flying hours 7020. 20 hours on Walter 601D turboprop engine and 430 hours Pratt & Whitney turbo-propeller engines.

Test Pilot CAA Class II. Mr Neil Thomas - 30 types: Piaggio P149D, total flying hours 6000. 80 hours experience on Walter 601D turboprop engine + 1300 hours on Pratt & Whitney turbo-propeller engines.

Aircraft Maintenance Organisation. Mr Johan Lok, (Warbirds, (Pty) Ltd).

Flight Test Management. The flight test programme was managed by the programme manager through a Safety Review Board (SRB). The SRB comprised following members:

1. Class I Test Pilot.
2. Class II Test Pilot.
3. Aircraft Maintenance Engineer.
4. CAA Certification representative.
5. Each flight planned + flight test card prepared prior to flight.
6. Hazard analysis conducted per flight – risks minimized through procedure or actions.





Conditions Relevant

- Aircraft Structural Limitations
 - Load factor: $N_z = +3.8g$. (Originally $+6g$ /reduced to $3.8g$ in accordance with static load tests approved by CAA).
 - Negative load factor: $N_z = -1.9g$. (FAR 23 negative limit $0.5 \times$ positive limit, i.e. $n = -1.9g$).
 - Retained:
 - Maximum speed: $V_D = 204$ KIAS.
 - MTOW (Normal Category): 1820 kgs.
 - Fwd CG limit: 0.42m.
 - Aft CG limit (Normal Category): 0.62 m.
- Mass and Balance. CG location each flight adjusted combination of long range fuel tank located aft and 30 kgs lead ballast located in baggage compartment.
- Test Schedule.
 - 7 July 2013 to 15 October 2014.
 - 54.9 hours flown; included 28 flight test hours and 10 owner conversion hours.
- Test Location. Wonderboom Airport, Pretoria, elevation 4095 feet, main runway 29/11, total distance 5996 ft asphalt surface.
- Air Traffic Control. Air Traffic Control and Fire/Emergency response provided by Wonderboom Airport.



Flight Test Programme

- Build-up to first flight
 - engine ground runs,
 - ground handling,
 - low speed and high speed taxi tests.
 - Build-up in torque vs handling qualities vs pilot workload.
- Airframe/engine structural inspections after every flight.
- Pitot/Static calibration.
- Engine In-Flight Relight.
- Stalling characteristics, level +accelerated flight (various flap/CG positions).
- Static and Dynamic Stability. Short Period Pitching Oscillation (SPPO)/Long period 'Phugoid'/-Longitudinal static stability.
- Lateral Directional. Dutch Roll/Spiral Stability/Steady Heading Sideslip.
- Manoeuvre Stability. Wind-up turns.
- Performance = Take-off /Climb performance/Level Cruise performance.
Descent performance/Landing performance.



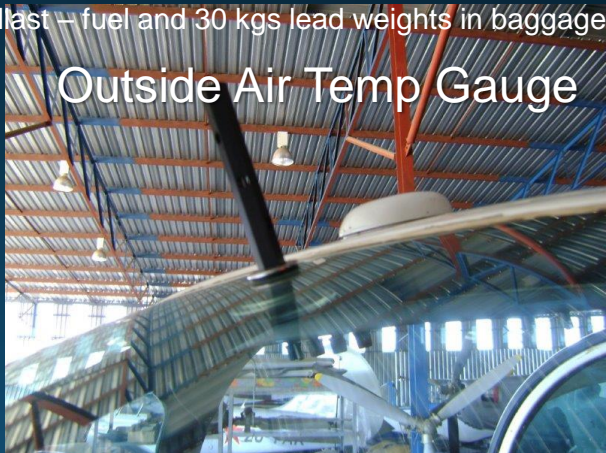
Flight Test Instrumentation



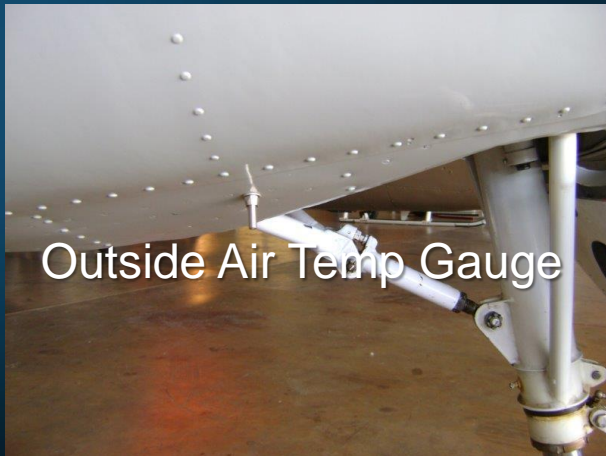
No automated flight test instrumentation was provided.

Test data manually recorded from aircraft's:

- Flight and engine instruments.
- Stick force gauge to measure stick forces
- Rudder forces estimated
- Sideslip strings to estimate sideslip angle.
- OAT
- Ballast – fuel and 30 kgs lead weights in baggage compartment



Outside Air Temp Gauge



Outside Air Temp Gauge



Rudder angular displacement tapeline.



Pitch and elevator control column displacement measurement.



Structural Testing



Cradle tested to 2 limit loading cases required by FAR 23.361 and 23.363.



A turbine torque factor of 1.6 and a factor of safety of 1.5 were included in load calcs

Inspections on critical airframe structure viz

- Engine mountings.
- Horizontal tail mounting structure.
- Inspections repeated every 5 operating hours up to 25 hours.
- Structural inspections continued every 25 hours to 100 hours and thereafter during MPI's.



Mass & Balance



	MASS (kgs)
WEIGH DATA:	
Nose wheel	214,0
L/H main wheel	547,0
R/H main wheel	554,1
SUB TOTALS:	1315,1
Fuel inboard fwd tanks (max 68 kg)	68
Fuel inboard rear tanks (max 118 kg)	118
Fuel centre tanks (max 142 kg)	0
Fuel tip tanks (max 60 kg)	60
Fuel auxiliary tank (max 56 kg)	56
TOTAL FUEL LOAD:	302
Pilot	85
Co-pilot	85
Pax (max 2)	0
Baggage (max 70 kg)	30
	1817,1

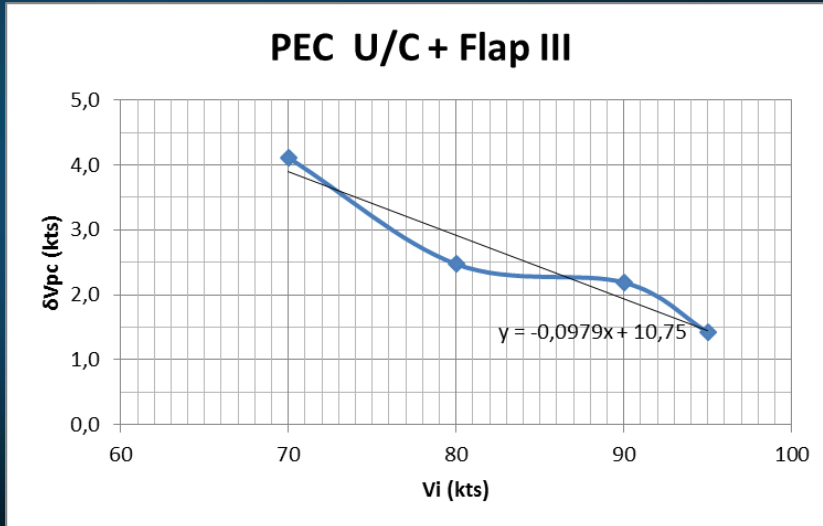
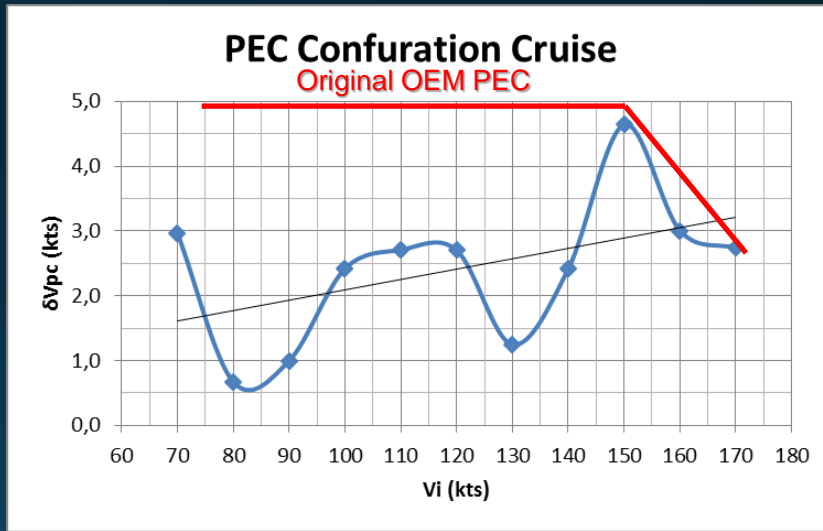
MAXIMUM TAKE-OFF MASS 1820 kg

FLYING CG RANGE: 0.424 m to 0.622 m



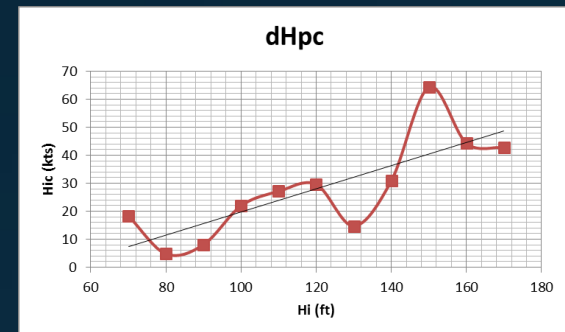


Pitot Statics – FAR 23.1323



- Nose extended by 305mm (12 inches).
- Reshaped canopy effects on flow field in vicinity of static ports.

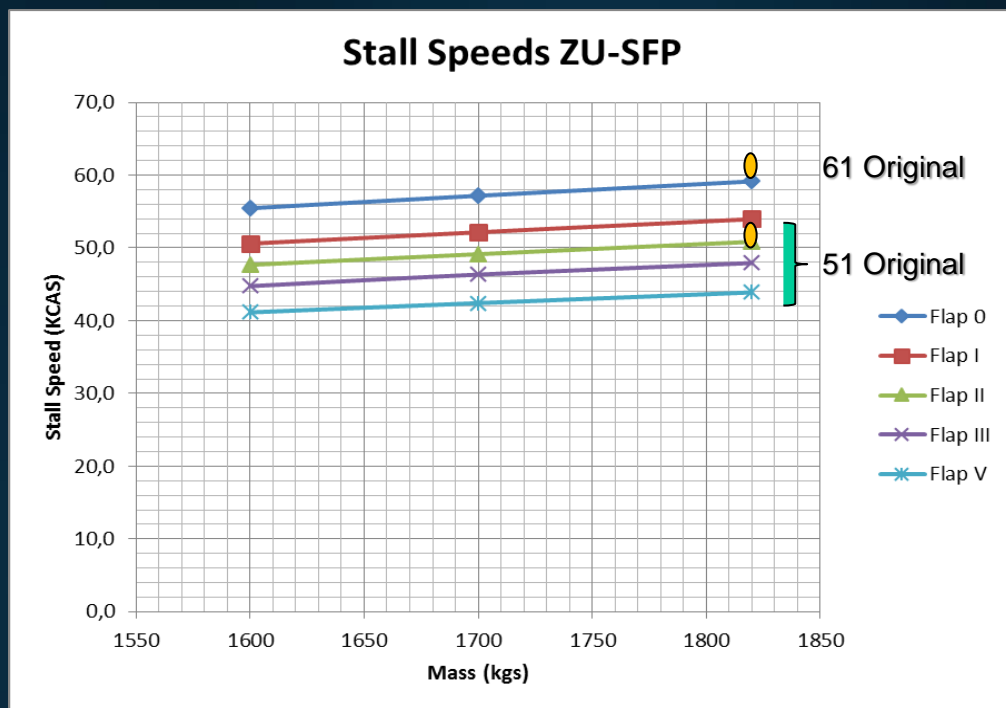
FAR 23.1323 = $\delta V_{pc} < 3\%$ or 5 kts, whichever greater from 1.3 V_{s1} to V_{ne}





Stalling: FAR 23.207

- Must be a clear and distinctive stall warning, flaps and U/C in normal position, in straight and level and turning flight.
- Stall warning margin of not less than 5 knots and must continue until stall occurs.
- Stall warning of 2 KIAS unsatisfactory.
- FAR Part 23.207 Stall Warning, was not complied with.
- 61 KCAS promulgated in FAR 23.49.c in which V_{so} and V_{s1} at maximum weight must not exceed 61 knots



Stall speeds lower than Piaggio P149D ranging

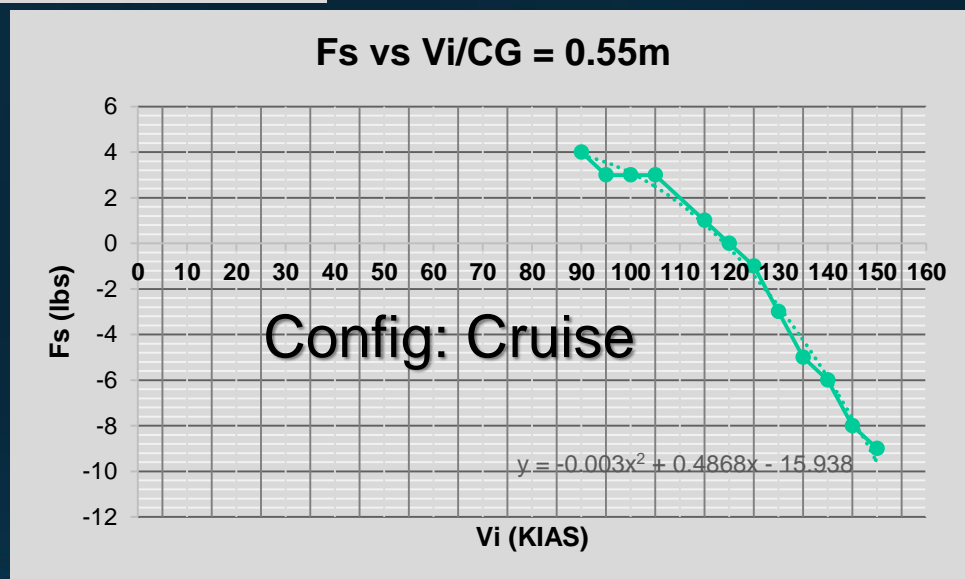
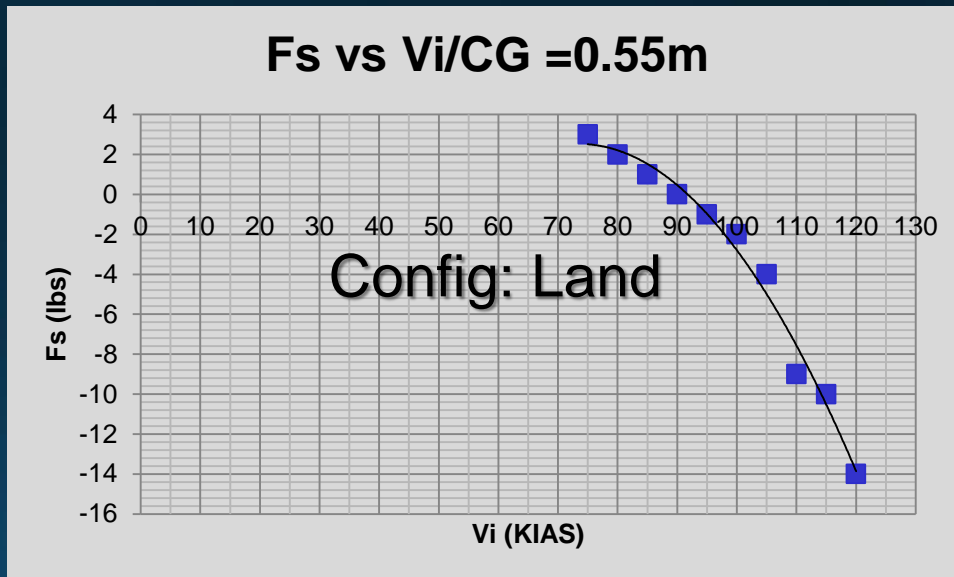
- 2 KIAS lower in cruise.
- 7 KIAS lower landing configuration ($C_{lmax} = 1.9$)

Contributory causes considered to be

- C_l from increased mass flow
- 'swooplets'



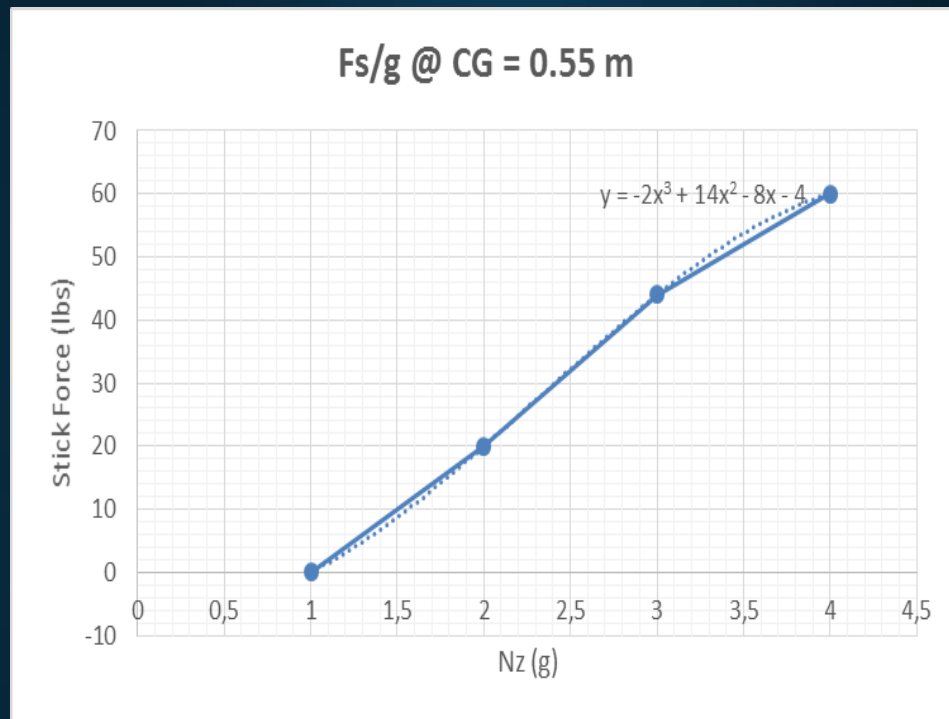
Longitudinal Static Stability: FAR Part 23.173





Manoeuvre Stability/CG = 0.55m

- Wind-up turns + pull-ups during accelerated stalls.
- Stick force/g increase linearly with increase in 'g'
- Maximum 60 lbs/g at V_a of 160 KIAS/ $N_z = 4g$ gradient of 15 lbs per g.
- FAR Part 23, Sec. 23.155 Elevator Control Force in Manoeuvres was complied with





Minimum Control Speed

- Minimum control speed/maximum torque airspeed determination.
- Determine boundary between aerodynamic control power versus asymmetric torque effects.
- Test conducted at 5,000 ft pressure altitude (5690 ft density altitude);
 - F_r did not exceed 150 pounds.
 - Not necessary to reduce power of the engine to maintain control.
 - Aircraft did not assume any dangerous attitude.
 - Possible to prevent heading change of more than 20° .

Configuration Cruise. DA = 5690 ft. Max torque 90 psi/100%/1970 RPM.

- $V_i = 65$ KIAS - aircraft fully controllable about all axes
- 4 units right rudder (50% of maximum)
- 2 units right aileron trim.



Configuration Landing.

- 2 x Compressor blowback @ 60 KIAS/ 2 due to engine acceleration and unstable intake conditions.
- Second attempt lower rate - aircraft controllable at 60 KIAS
- Maximum right rudder
- 1/2 aileron; rate of asymmetry controllable.
- Recommended 'wave-off' minimum airspeed = 60 KIAS (15 KIAS margin/MAUW)
- **Essential: pilots NOT TO SLAM THE POWER LEVER OPEN at low speeds/high angles of attack.**



Trimmability: Landing Configuration

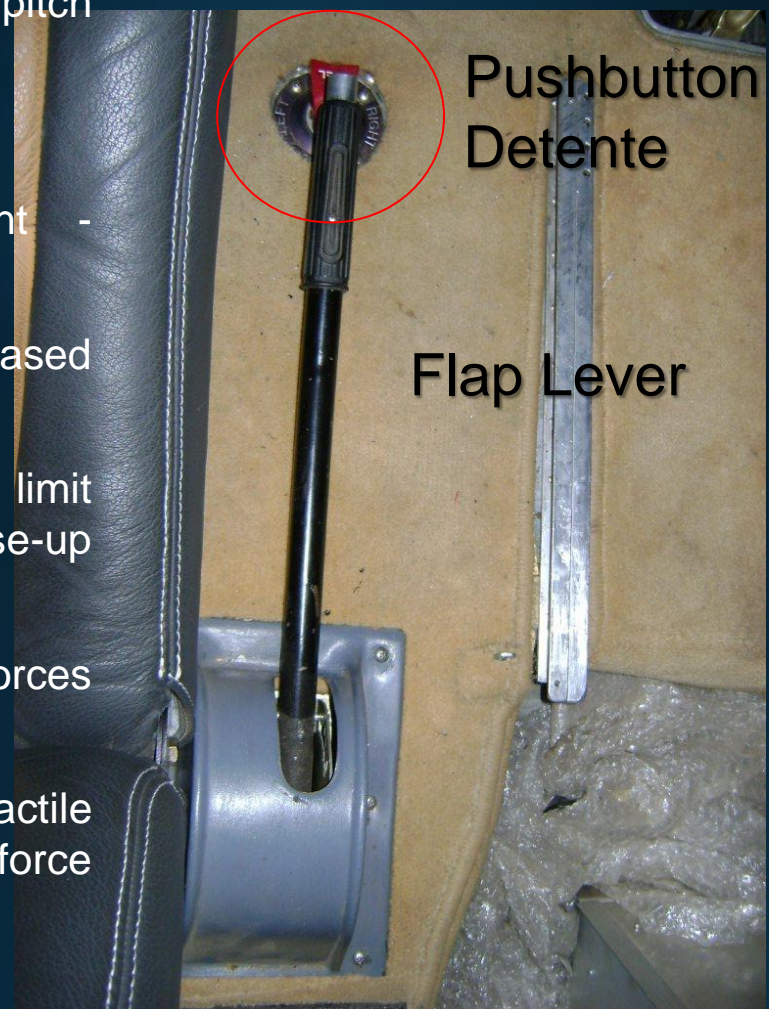
Insufficient trim authority to trim the aircraft in pitch with flap settings greater than Flap III.

- Effect of flap extension – CP moves aft,
- Increased nose-down pitching moment - requires nose-up trim.
- Decreased tailplane authority due to increased downwash.

Additional trim authority to maximum allowable limit setting provided by increasing the trim motor nose-up deflection.

Approaches >Flap III, residual stick forces approximately 8 lbs pull required for approach.

Unsatisfactory but acceptable; provided tactile feedback for landing flare without excessive pull force required.





Performance Comparison

MAUW 1820 kgs



Parameter	P149D	P149D TP
Takeoff Distance 50 ft (ISA +13°C)	2420 ft	1180 ft
Stall Speed (KIAS)	51	45
Crosswind Limit (kts)	20	20
Climb Time (mins) 5,000 ft – 10,000 ft	7.0	2.0
Ceiling (ft) ISA* (150 ft/min)	14,000	21,000 (extrapolation)
Power/Weight Ratio	0.14	0.4
Fuel Used in Climb	9.1 litres	8 litres
Descent Best Glide Speed (90 KIAS)	1.2 nms/1000 ft	2.86 nms/1000 ft prop feathered

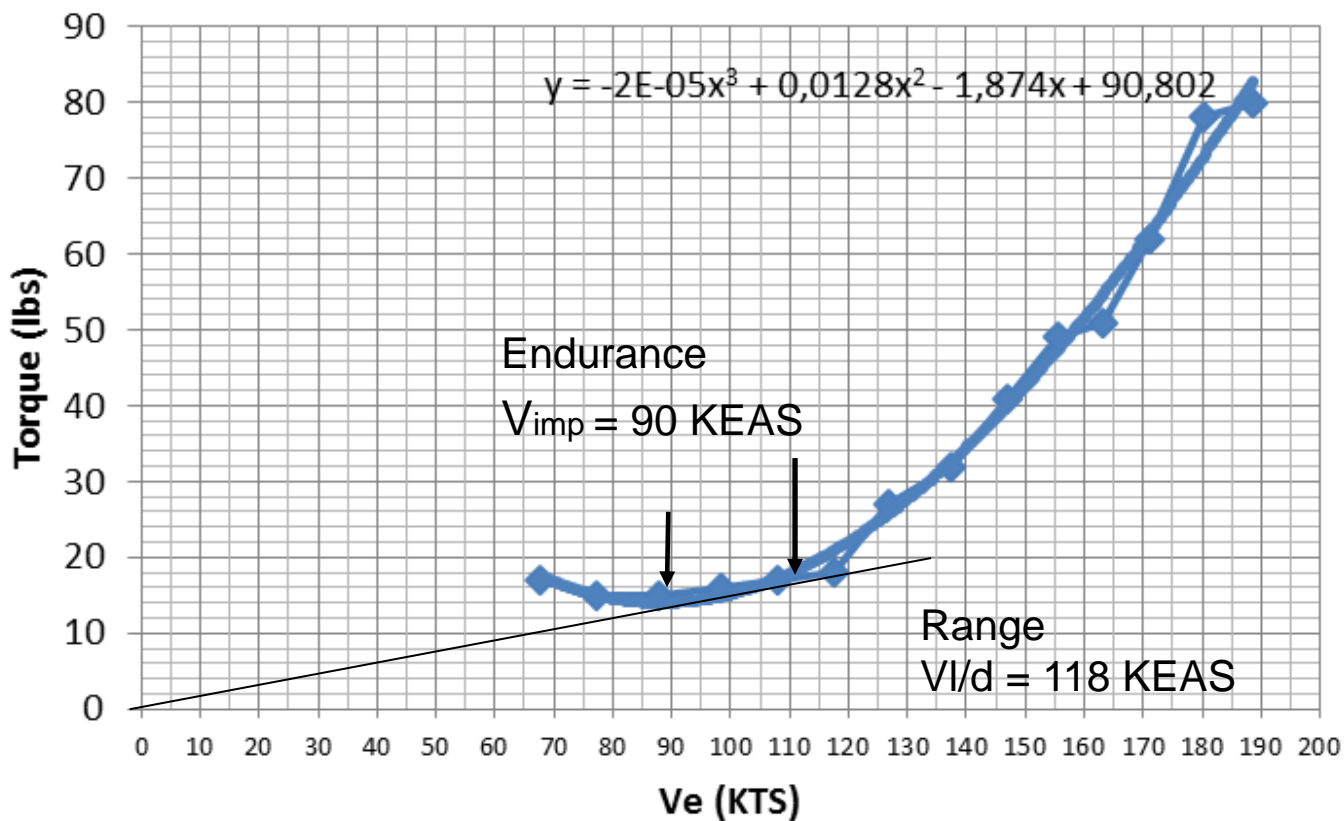
SEP climb profile airspeed conversion rate of 10 KIAS per 1000 ft

- average rate of climb 2542 ft/min +
- pitch attitude approximately 17°,
- high workload for the pilot.



Level Cruise Performance

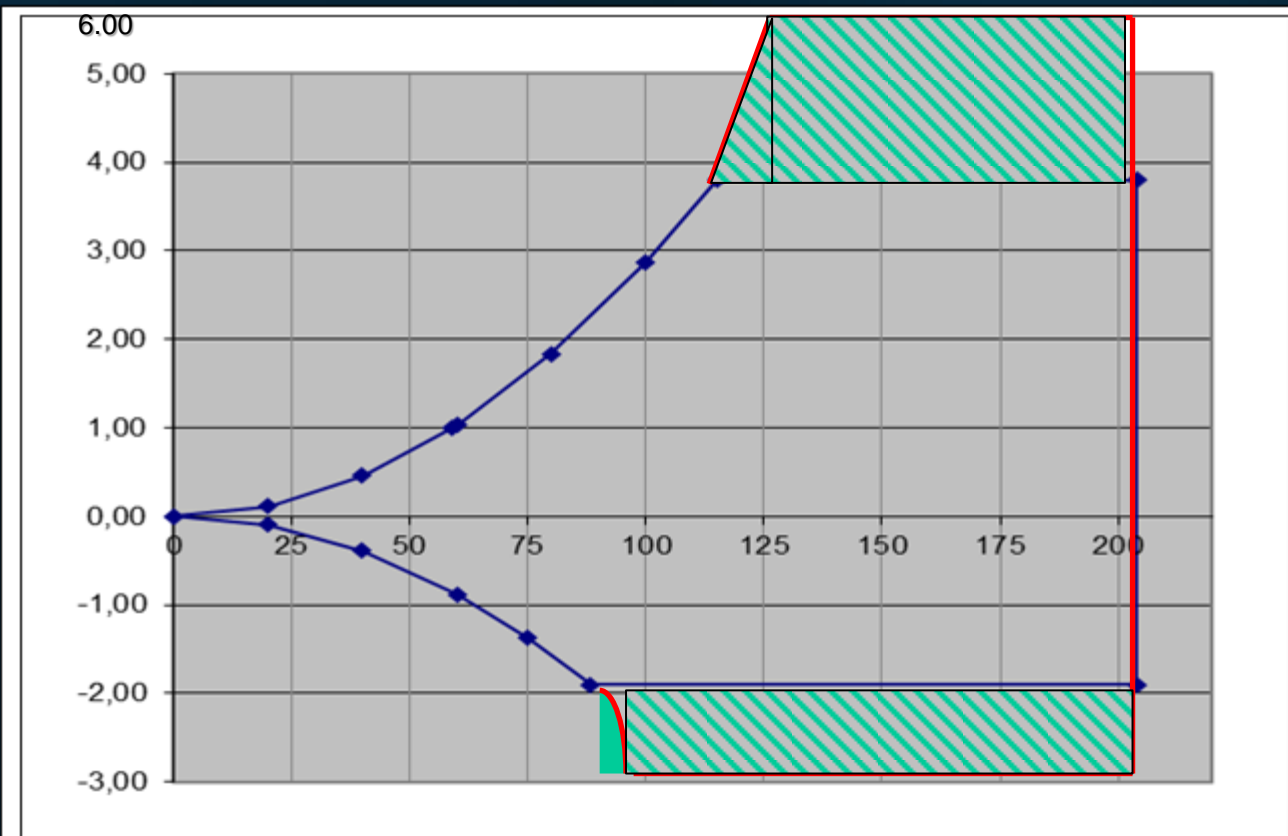
Power Required/8000 ft Pressure Alt/ISA/1820
kgs





Vn Diagram

Nz



Vn diagram for *Piaggio P149D TP*.

Vi (KIAS)

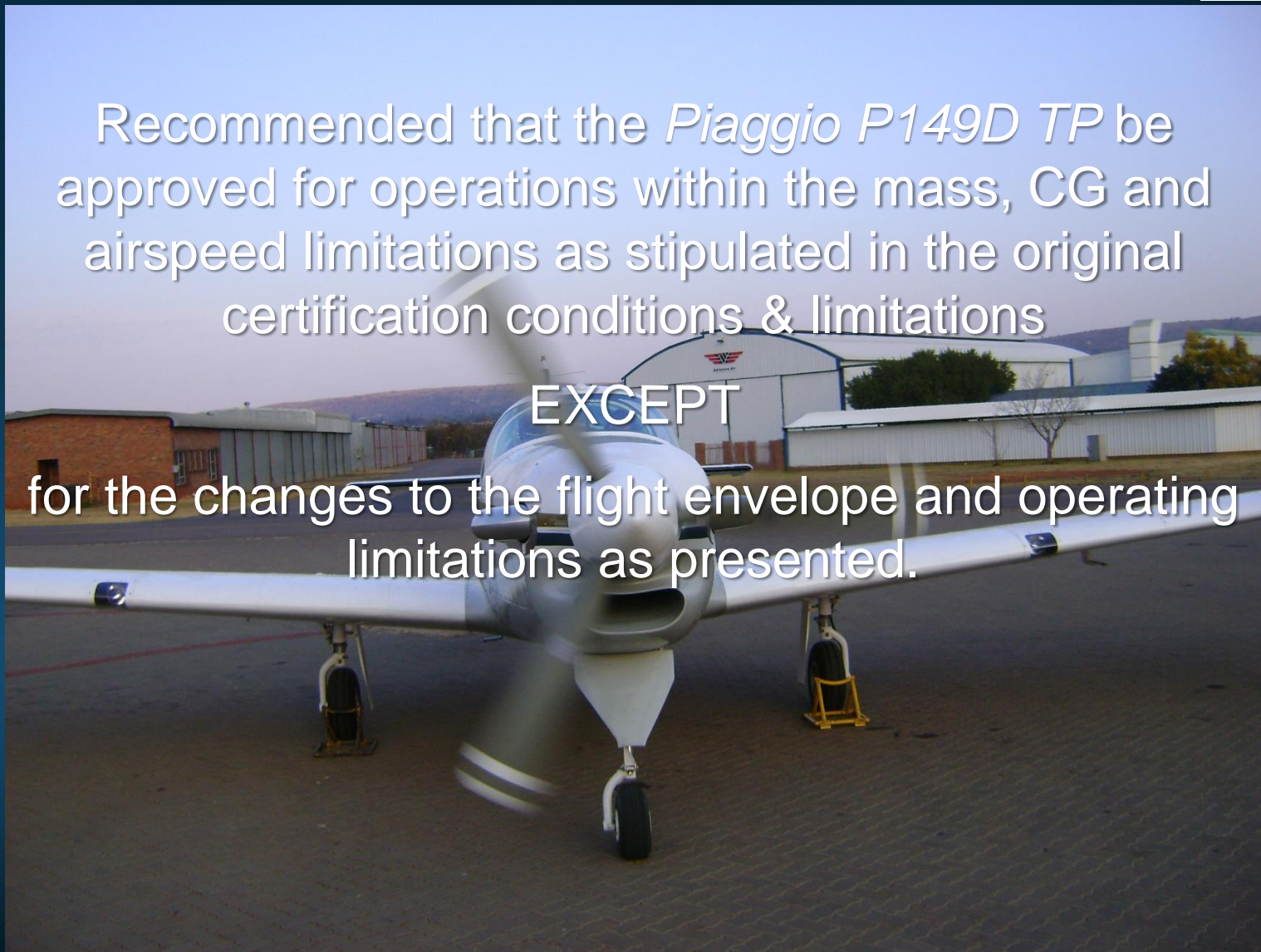


Recommendations

Recommended that the *Piaggio P149D TP* be approved for operations within the mass, CG and airspeed limitations as stipulated in the original certification conditions & limitations

EXCEPT

for the changes to the flight envelope and operating limitations as presented.





Thank You!



The happy owner
Werner Heiml