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## FUEL RESEARCH INSTITUTE

OF SOUTH AFRICA

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TECHNICAL

NO. 33 OF 1973

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### DENSITY AND OXYGEN CONTENT OF MOIST AIR

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DENSITY AND OXYGEN CONTENT OF MOIST AIR

1. The normal ambient air always contains some water vapour. Its presence has two effects:
  - i) It acts as a diluent and reduces the concentration of the constituents of dry air, that of the oxygen content being usually the most important aspect;
  - ii) As water vapour is less dense than air, the density of moist air is less than that of dry air.

A knowledge of the density is required for the evaluation of air-flow measurements involving orifice plates, pitot tubes and similar equipment. The oxygen content must be known when the air requirements of a combustion process have to be computed.

At the temperature and humidity normally prevailing in Pretoria, the density correction will normally not exceed 1%, which in most cases is hardly significant. At higher temperatures and humidities, the effect on the density and oxygen concentration can be appreciable and has to be taken into consideration.

2. If the atmosphere contains water vapour, the total absolute pressure  $B$  is the sum of the partial pressures of the air,  $p_a$ , and of the water vapour,  $p$ . The maximum value of  $p$  is the saturation pressure  $p_s$ , which depends on the temperature according to a relation represented by the attached tables and diagrams.

The actual value of  $p$  can then be expressed as

$$p = \Phi p_s \quad (1)$$

where  $\Phi$  is the relative humidity, a figure between 0 and 1, usually expressed as a percentage.

The mass of water which can exist in the vapour state within a given volume is likewise a maximum at saturation and is, per cubic metre, equal to  $\rho_s$  ( $\text{kg/m}^3$ ). The actual quantity  $x$  ( $\text{kg/m}^3$ ) can then be expressed as

$$x = \beta \rho_s \quad (2)$$

where  $\beta$  is the saturation factor.

$\beta$  is related to  $\Phi$  by the equation

$$\beta = \Phi \frac{B - p_s}{B - p} \quad (3)$$

In most cases,  $p_s$  and  $p$  are considerably smaller than  $B$ , in which case (and also when  $p \approx p_s$ )

$$\beta = \Phi$$

$\rho_s$  is, like  $p_s$ , a function of the temperature. Data are indicated in the tables and figures.

In the range  $0^\circ\text{C}$  to  $40^\circ\text{C}$ , the expression

$$\rho_s = 9,6 \times 10^{-4} p_s, \text{ or even } \rho_s = 10^{-3} p_s$$

is sufficiently accurate for most purposes.

The mass of  $1\text{m}^3$  of moist air, or in other words its density  $\rho$ , obviously equals

$$\rho = \rho_d + x \quad (\text{kg/m}^3)$$

where  $\rho_d$  is the mass of  $1\text{m}^3$  of dry air of partial pressure  $p_a = B - p$  at the prevailing temperature  $t(\text{ }^\circ\text{C})$ .

The density of air at a pressure of 760 mm mercury ( $101325 \text{ N/m}^2$  or  $10332,3 \text{ kgf/m}^2$ ) equals

$$\rho_0 = 1,2928 \text{ kg/m}^3$$

/The .....

The density of dry air at the temperature  $T = t + 273,16\text{ (K)}$  and pressure  $D_a$  (mm Hg) consequently equals

$$\rho_d = 1,2928 \frac{D_a}{760} \frac{273,16}{T} = 0,46466 \frac{p_a}{T}$$

The exact expression for the density  $\rho$  of moist air is thus

$$\begin{aligned} \rho &= 0,46466 \frac{B - p}{T} + x = \\ &0,46466 \frac{B - \Phi p_s}{T} + \Phi \rho_s \frac{B - p_s}{B - \Phi p_s} \end{aligned} \quad (4)$$

In many cases, and certainly when  $t \leq 40^\circ\text{C}$ , this may be simplified to

$$\begin{aligned} \rho &= 0,4647 \frac{B}{T} - 0,4647 \frac{\Phi p_s}{T} + 10^{-3} \Phi p_s, \text{ or} \\ \rho &= 0,4647 \frac{B}{T} - \left( \frac{0,465}{T} - 0,001 \right) \Phi p_s \\ \rho &= \rho(B, T) - \Phi f \end{aligned} \quad (5)$$

The first term  $\rho(B, T)$  is the density of dry air at the ambient temperature and total pressure, as indicated by a barometer, which may be derived from tables Nos. 2 or 3. The second term  $\Phi f$  is a correction factor depending only on the temperature and humidity; the value of  $f$  is indicated in Table No. 1 and figure No. 3.

The mass of dry air actually present in  $1\text{m}^3$ , or  $\rho_d$ , is less than  $\rho(B, T)$  and follows from

$$\rho_d = \rho(B, T) \frac{B - \Phi p_s}{B}$$

The concentrations of the constituents of dry air, as those of nitrogen, oxygen, etc., are likewise reduced by the factor

$$K = \frac{B - \Phi p_s}{B}$$

/Some .....

Some examples, illustrating the foregoing and indicating the magnitude of the corrections, follow hereunder.

Examples.

1.  $B = 650 \text{ mm Hg}, t = 25^\circ\text{C} \quad \Phi = 50\%.$

Table No. 2 supplies  $p_s = 24,2 \text{ mm Hg}$ ,  $f = 14 \times 10^{-3}$ , while Table No. 3 indicates  $\rho(B,T) = 1,013 \text{ kg/m}^3$ . The actual density thus equals  $\rho = 1,013 - 0,007 = 1,006$ . The factor  $K = \frac{650 - 12,1}{650} = 0,98$

The correction to the density is thus, for most purposes, hardly significant. The oxygen concentration is reduced to  $0,98 \times 21 = 20,6\%$ . For technical applications, this is not of much interest. However, if one calibrates a magnetic oxygen meter with ambient air, the deviation is of sufficient magnitude to be taken into consideration.

2. A wet blast gas producer is operated with air, saturated at  $55^\circ\text{C}$ ,  $650 \text{ mm Hg}$ .

From Table No. 1 :  $p_s = 118 \text{ mm Hg}, \rho_w = 0,104 \text{ kg/m}^3$ .  
From eq. (4)

$$\rho = 0,46466 \frac{532}{328,16} + 0,104 = 0,754 + 0,104 = 0,858 \text{ kg/m}^3$$

$$K = \frac{532}{650} = 0,82.$$

The density of dry air at  $650 \text{ mm Hg}$ ,  $55^\circ\text{C}$ , would have been  $\rho(B,T) = 0,920 \text{ kg/m}^3$ .

The oxygen content of the wet blast equals  $0,82 \times 21 = 17,2\%$ . The moisture content of the wet blast is  $\frac{104}{858} \cdot 100 = 12,1\%$  by weight.

In this case, the effect of the water vapour on density and oxygen content is appreciable.

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CHIEF RESEARCH OFFICER

Pretoria.  
19th June, 1973.  
GAWvD/EMc

TABLE NO. 1

PROPERTIES OF WATER VAPOUR

| Temp.<br>°C | Saturation Pressure |                  |                    | Density<br>g/m <sup>3</sup> | Correction<br>-f |
|-------------|---------------------|------------------|--------------------|-----------------------------|------------------|
|             | mm Hg               | N/m <sup>2</sup> | kgf/m <sup>2</sup> |                             |                  |
| 0           | 4,58                | 611              | 62,28              | 4,85                        | 0,003            |
| 5           | 6,54                | 872              | 88,90              | 6,80                        | 0,005            |
| 10          | 9,20                | 1227             | 125,13             | 9,40                        | 0,006            |
| 15          | 12,78               | 1704             | 173,76             | 12,82                       | 0,008            |
| 20          | 17,53               | 2337             | 238,3              | 17,29                       | 0,011            |
| 25          | 23,75               | 3167             | 322,9              | 23,64                       | 0,014            |
| 30          | 31,81               | 4241             | 432,5              | 30,36                       | 0,018            |
| 35          | 42,17               | 5623             | 573,5              | 39,60                       | 0,023            |
| 40          | 55,31               | 7375             | 752,0              | 51,14                       | 0,029            |
| 45          | 71,87               | 9582             | 977,1              | 65,44                       |                  |
| 50          | 92,52               | 12335            | 1258               | 82,98                       |                  |
| 55          | 118,1               | 15740            | 1605               | 104,3                       |                  |
| 60          | 149,4               | 19920            | 2031               | 130,2                       |                  |
| 65          | 187,5               | 25010            | 2550               | 161,1                       |                  |
| 70          | 233,7               | 31150            | 3177               | 198,1                       |                  |
| 75          | 289,2               | 38550            | 3931               | 241,8                       |                  |
| 80          | 355,2               | 47360            | 4829               | 293,3                       |                  |
| 85          | 433,5               | 57800            | 5894               | 353,4                       |                  |
| 90          | 525,9               | 70110            | 7149               | 423,5                       |                  |

An approximate equation for ps (in mmHg) is

$$\log ps = 8,8730 - \frac{2241,14}{T}$$

TABLE NO. 2

DENSITY OF DRY AIR

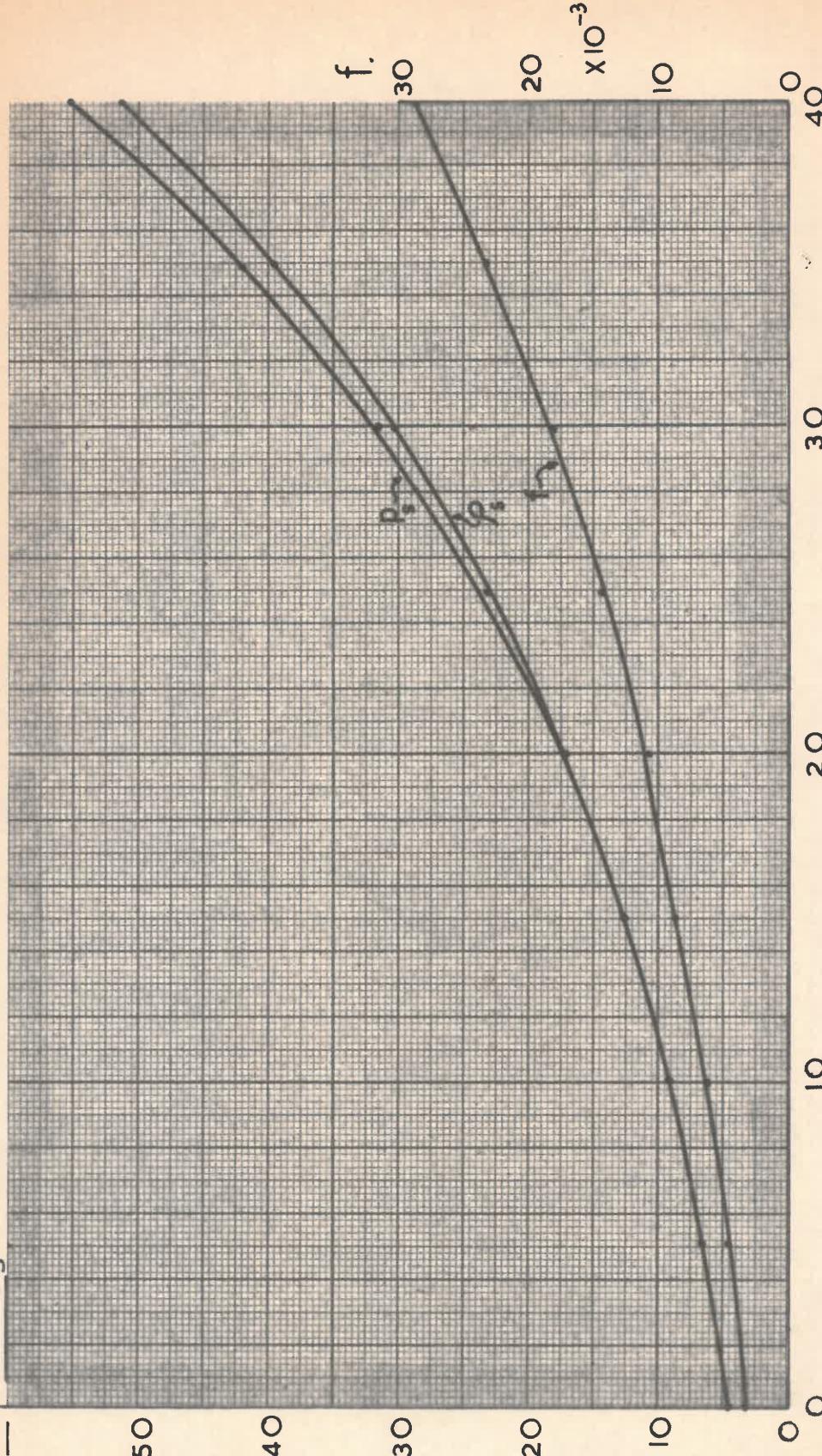
| B<br>mm Hg | Temperature, °C |       |       |       |       |       |       |       |       |  |
|------------|-----------------|-------|-------|-------|-------|-------|-------|-------|-------|--|
|            | 0               | 5     | 10    | 15    | 20    | 25    | 30    | 35    | 40    |  |
| 640        | 1,089           | 1,069 | 1,050 | 1,032 | 1,014 | 0,997 | 0,981 | 0,965 | 0,950 |  |
| 645        | 1,097           | 1,078 | 1,059 | 1,040 | 1,022 | 1,005 | 0,989 | 0,973 | 0,957 |  |
| 650        | 1,106           | 1,086 | 1,067 | 1,048 | 1,030 | 1,013 | 0,996 | 0,980 | 0,965 |  |
| 655        | 1,114           | 1,094 | 1,075 | 1,056 | 1,038 | 1,021 | 1,004 | 0,988 | 0,972 |  |
| 660        | 1,123           | 1,103 | 1,083 | 1,064 | 1,046 | 1,029 | 1,012 | 0,995 | 0,979 |  |
| 665        | 1,131           | 1,111 | 1,091 | 1,072 | 1,054 | 1,036 | 1,019 | 1,003 | 0,987 |  |
| 670        | 1,140           | 1,119 | 1,100 | 1,080 | 1,062 | 1,044 | 1,027 | 1,010 | 0,994 |  |
| 675        | 1,148           | 1,128 | 1,108 | 1,089 | 1,070 | 1,052 | 1,035 | 1,018 | 1,002 |  |
| 680        | 1,157           | 1,136 | 1,116 | 1,097 | 1,078 | 1,060 | 1,042 | 1,025 | 1,009 |  |
| 685        | 1,165           | 1,144 | 1,124 | 1,105 | 1,086 | 1,068 | 1,050 | 1,033 | 1,016 |  |
| 690        | 1,174           | 1,153 | 1,132 | 1,113 | 1,094 | 1,075 | 1,058 | 1,041 | 1,024 |  |
| 695        | 1,182           | 1,161 | 1,141 | 1,121 | 1,102 | 1,083 | 1,065 | 1,048 | 1,031 |  |
| 700        | 1,191           | 1,169 | 1,149 | 1,129 | 1,110 | 1,091 | 1,073 | 1,056 | 1,039 |  |
| 705        | 1,199           | 1,178 | 1,157 | 1,137 | 1,118 | 1,099 | 1,081 | 1,063 | 1,046 |  |
| 710        | 1,208           | 1,186 | 1,165 | 1,145 | 1,125 | 1,107 | 1,088 | 1,071 | 1,054 |  |
| 715        | 1,216           | 1,194 | 1,173 | 1,153 | 1,133 | 1,114 | 1,096 | 1,078 | 1,061 |  |
| 720        | 1,225           | 1,203 | 1,182 | 1,161 | 1,141 | 1,122 | 1,104 | 1,086 | 1,068 |  |
| 725        | 1,233           | 1,211 | 1,190 | 1,169 | 1,149 | 1,130 | 1,111 | 1,093 | 1,076 |  |
| 730        | 1,242           | 1,220 | 1,198 | 1,177 | 1,157 | 1,138 | 1,119 | 1,101 | 1,083 |  |
| 735        | 1,250           | 1,228 | 1,206 | 1,185 | 1,165 | 1,146 | 1,127 | 1,108 | 1,091 |  |
| 740        | 1,259           | 1,236 | 1,214 | 1,193 | 1,173 | 1,153 | 1,134 | 1,116 | 1,098 |  |
| 745        | 1,267           | 1,245 | 1,223 | 1,201 | 1,181 | 1,161 | 1,142 | 1,123 | 1,106 |  |
| 750        | 1,276           | 1,253 | 1,231 | 1,209 | 1,189 | 1,169 | 1,150 | 1,131 | 1,113 |  |
| 755        | 1,284           | 1,261 | 1,239 | 1,218 | 1,197 | 1,177 | 1,157 | 1,139 | 1,120 |  |
| 760        | 1,293           | 1,270 | 1,247 | 1,226 | 1,205 | 1,185 | 1,165 | 1,146 | 1,128 |  |
| 765        | 1,301           | 1,278 | 1,255 | 1,234 | 1,213 | 1,192 | 1,173 | 1,154 | 1,135 |  |
| 770        | 1,310           | 1,286 | 1,264 | 1,242 | 1,221 | 1,200 | 1,180 | 1,161 | 1,143 |  |

TABLE NO. 3

DENSITY OF DRY AIR

| B<br>mm Hg | Temperature, °C |       |       |       |       |       |       |       |       |
|------------|-----------------|-------|-------|-------|-------|-------|-------|-------|-------|
|            | 20              | 21    | 22    | 23    | 24    | 25    | 26    | 27    | 28    |
| 640        | 1,014           | 1,011 | 1,008 | 1,004 | 1,001 | 0,997 | 0,994 | 0,991 | 0,988 |
| 641        | 1,016           | 1,013 | 1,009 | 1,006 | 1,002 | 0,999 | 0,996 | 0,992 | 0,989 |
| 642        | 1,018           | 1,014 | 1,011 | 1,007 | 1,004 | 1,001 | 0,997 | 0,994 | 0,991 |
| 643        | 1,019           | 1,016 | 1,012 | 1,009 | 1,006 | 1,002 | 0,999 | 0,995 | 0,992 |
| 644        | 1,021           | 1,017 | 1,014 | 1,010 | 1,007 | 1,004 | 1,000 | 0,997 | 0,994 |
| 645        | 1,022           | 1,019 | 1,015 | 1,012 | 1,009 | 1,005 | 1,002 | 0,999 | 0,995 |
| 646        | 1,024           | 1,021 | 1,017 | 1,014 | 1,010 | 1,007 | 1,003 | 1,000 | 0,997 |
| 647        | 1,026           | 1,022 | 1,019 | 1,015 | 1,012 | 1,008 | 1,005 | 1,002 | 0,998 |
| 648        | 1,027           | 1,024 | 1,020 | 1,017 | 1,013 | 1,010 | 1,007 | 1,003 | 1,000 |
| 649        | 1,029           | 1,025 | 1,022 | 1,018 | 1,015 | 1,012 | 1,008 | 1,005 | 1,001 |
| 650        | 1,030           | 1,027 | 1,023 | 1,020 | 1,016 | 1,013 | 1,010 | 1,006 | 1,003 |
| 651        | 1,032           | 1,028 | 1,025 | 1,021 | 1,018 | 1,015 | 1,011 | 1,008 | 1,005 |
| 652        | 1,034           | 1,030 | 1,027 | 1,023 | 1,020 | 1,016 | 1,013 | 1,009 | 1,006 |
| 653        | 1,035           | 1,032 | 1,028 | 1,025 | 1,021 | 1,018 | 1,014 | 1,011 | 1,008 |
| 654        | 1,037           | 1,033 | 1,030 | 1,026 | 1,023 | 1,019 | 1,016 | 1,013 | 1,009 |
| 655        | 1,038           | 1,035 | 1,031 | 1,028 | 1,024 | 1,021 | 1,017 | 1,014 | 1,011 |
| 656        | 1,040           | 1,036 | 1,033 | 1,029 | 1,026 | 1,022 | 1,019 | 1,016 | 1,012 |
| 657        | 1,041           | 1,038 | 1,034 | 1,031 | 1,027 | 1,024 | 1,021 | 1,017 | 1,014 |
| 658        | 1,043           | 1,039 | 1,036 | 1,032 | 1,029 | 1,026 | 1,022 | 1,019 | 1,015 |
| 659        | 1,045           | 1,041 | 1,038 | 1,034 | 1,031 | 1,027 | 1,024 | 1,020 | 1,017 |
| 660        | 1,046           | 1,043 | 1,036 | 1,032 | 1,029 | 1,025 | 1,022 | 1,018 | 1,015 |

$\rho_{\text{g}/\text{m}^3}$  |  $P_{\text{mmHg}}$ .



SATURATION PRESSURE AND DENSITY OF WATER VAPOUR.

CORRECTION FACTOR. - f